

# DEEP FOUNDATIONS

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# Pile Parameters from Driving Analysis: Hiley Formula

$$R(S+c/2) = \eta W_h h$$

**R** = pile resistance

**S** = pile set

**c** = temporary elastic compression

**$\eta$**  = efficiency factor

**$W_h$**  = hammer weight

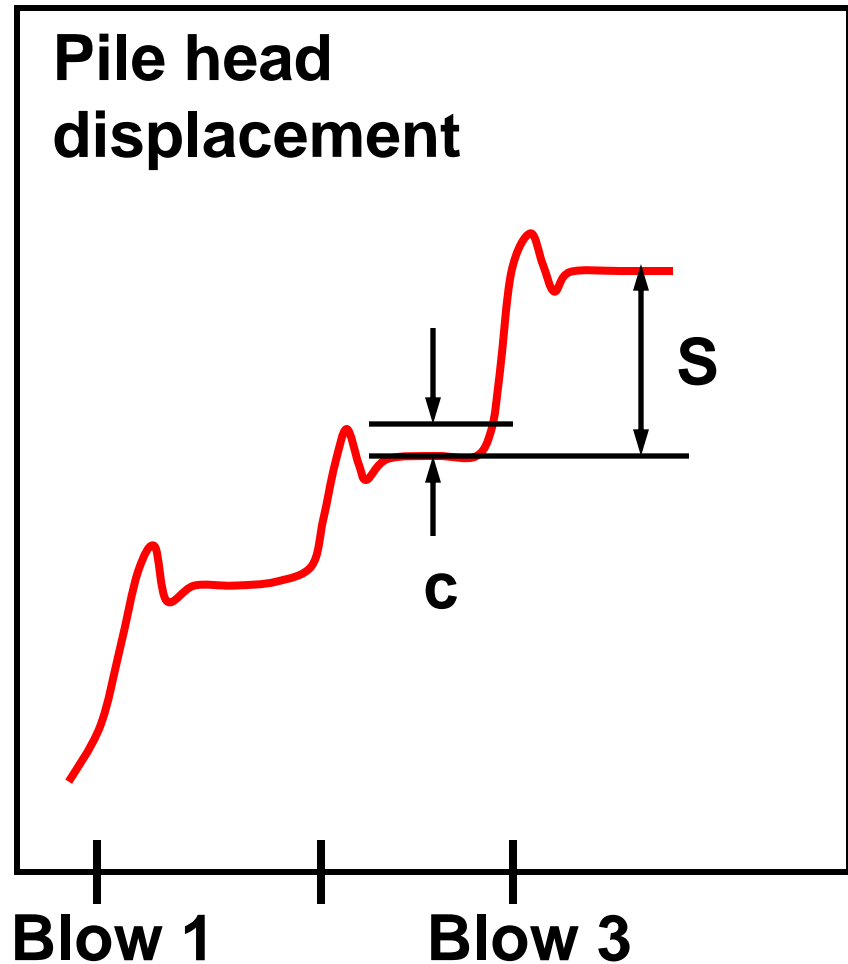
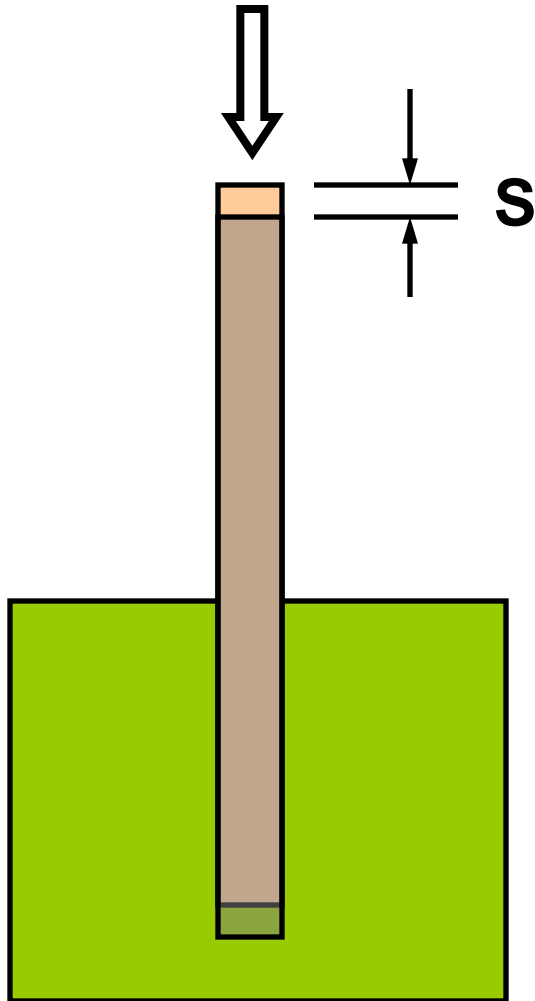
**h** = drop height

# Temporary Elastic Compression

- Temporary elastic compression includes:
  - Elastic compression of pile ,  $C_p$
  - Elastic compression of Soil,  $C_q$
  - Elastic compression of Pile driving cap,  $C_c$
- Note:

**Refer to E.C.P for estimation of elastic compression**

# Energy IN = Energy OUT



# *The efficiency factor*

$$\eta = \frac{k(W_h + e^2 W_p)}{W_h + W_p} \quad \square$$

$W_p$  = pile weight

$e$  = coefficient of 'restitution'

$k$  = output efficiency of the hammer

## Note:

Refer to E.C.P for  $e$  and  $k$

# The Hiley Formula

- Simple expression
- Requires driving efficiency of system
- Requires simple measurement of pile displacement near design depth, for regulated driving energy.

**WARNING:**

**Good record in sands, not so good in clays**

# Remaining Design Considerations

- Negative Skin Friction  
“downdrag forces on piles”
- Group action
- Settlement

# 1. Negative Skin friction

**Adhesion factor may be negative!**

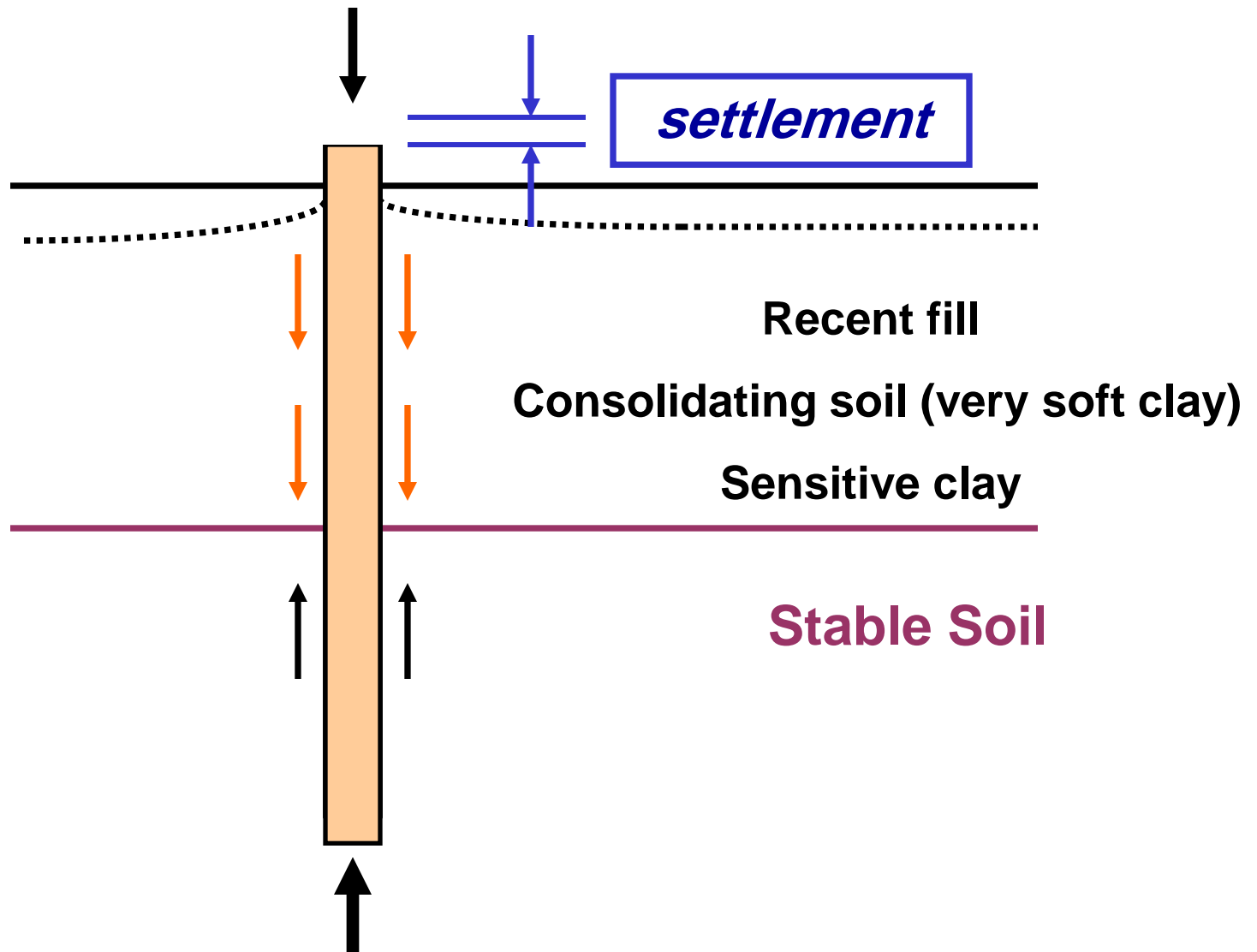
CRAIG - for NC clay undergoing consolidation

$$f_s = K_s (\sigma'_o) \tan \phi'$$

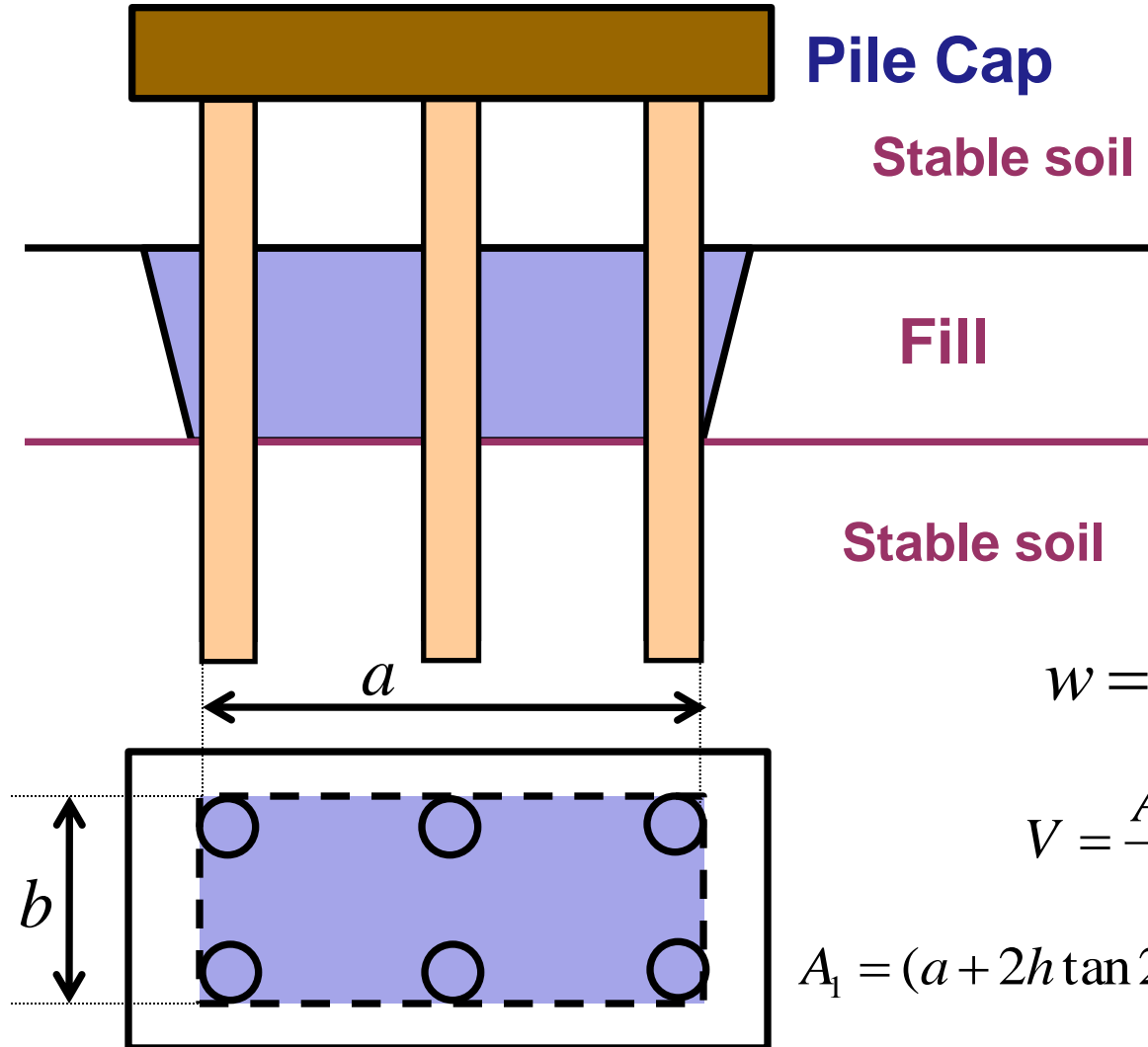
$$f_s \cong -0.25 \sigma'_o$$



# The Situation



# Estimation of Downdrag force



$$w = \gamma * V$$

$$V = \frac{A_1 + A_2}{2} h$$

$$A_1 = (a + 2h \tan 20) * (b + 2h \tan 20)$$

# Estimation of Downdrag force

## Steps for design:

- Estimate single pile capacity
- Calculate the required number of piles,  $N$
- Increase number of piles by one (for downdrag force due to negative skin friction),  $N_1$
- Draw the arrangement of piles
- Estimate the downdrag force as before
- Check the number of required piles

$$N = \frac{P_{F.L.} + W}{P_{all}} < N_1$$

## 2. PILE GROUPS

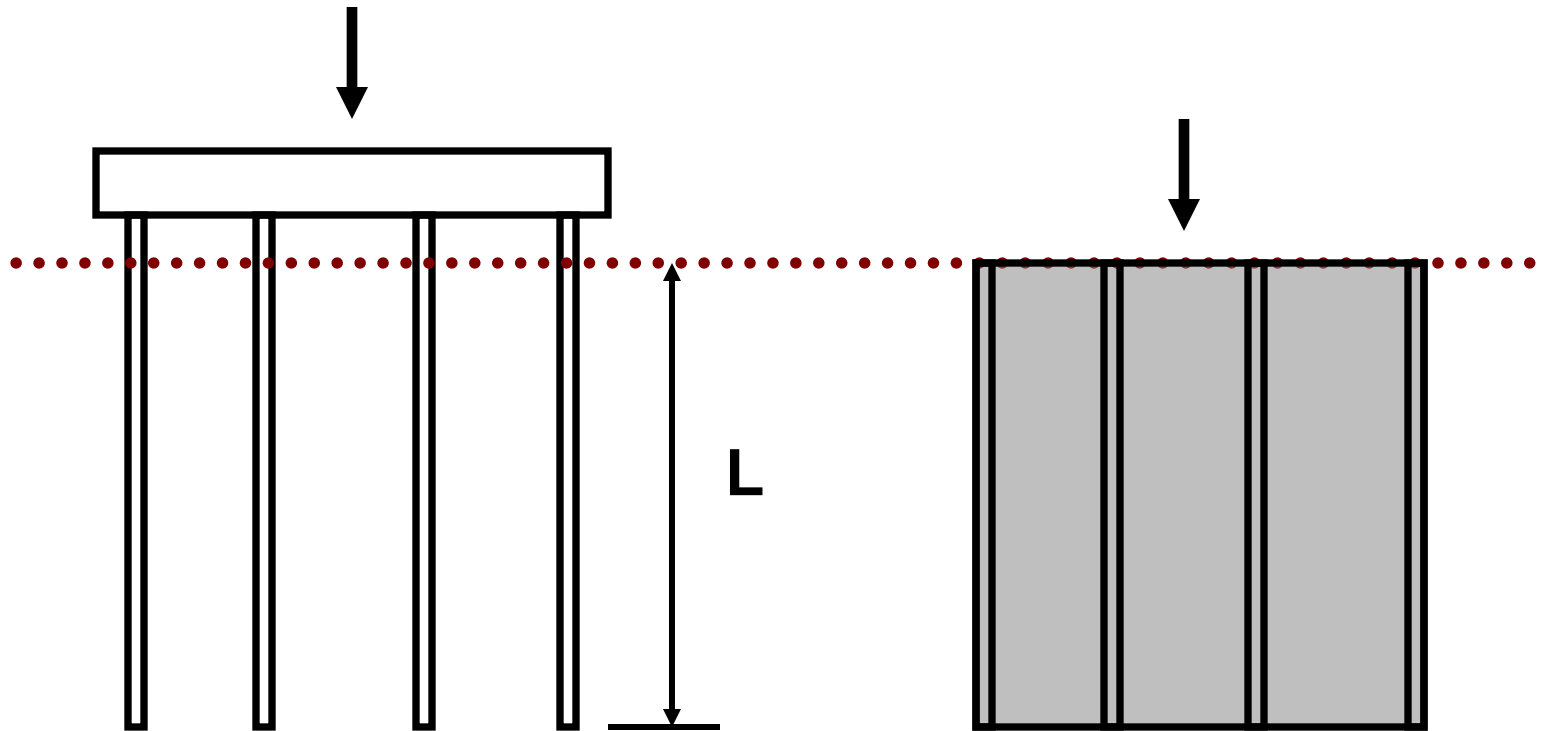
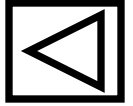
### Group “efficiency”

Group capacity not always =  $\Sigma$ (pile capacities)

RATIO of group to  $\Sigma$ (pile capacities) = ***EFFICIENCY,  $\eta$***

- close spacings in loose sand are ***efficient***
- close spacings in clay are ***inefficient***
- “**Block Action**” may determine Group capacity

# Block Action



4x4 pile group, dia.  $d$ ,  
spacing,  $s$

Block base,  $A_G = (3s + d)^2$ ,  
Perimeter,  $Per_G = 4(3s + d)L$

# Calculations

- **For design,**
- Check the capacity of group is **greater** than  $\Sigma(\text{pile capacities})$

$$P_{G_{all}} = \frac{P_{G_{ult}}}{F.S.} = \frac{CN_c A_G + C_a L^* Per_G}{F.S.}$$

$$P_{F.L.} + w \leq P_{G_{all}} \quad \eta = \frac{P_{G_{all}}}{P_{F.L.} + w} \geq 1.00$$

**NOTE:** *unlikely to need except for close piles in saturated clays,  $s < 4d$*

# PILES - SUMMARY

Pile capacity depends largely on installation

## 1. Single Piles (a) STATIC ANALYSIS

Sands:  $f_{smax}$  and  $f_{bmax}$

Clays - adhesion factor,  $\alpha$

$$- f_b = 9c_u$$

## (b) CPT DATA

- better parameter evaluation

# SUMMARY

## 1. Single Piles      (c) Dynamic Analysis

“driving” data used  
(gives capacity at the  
time of pile-driving)

## 2. Pile Groups

**Block Action** may  
diminish capacity, AND  
increase settlement