

### **EX2:** Hydrostatic Forces on Completely Submerged Curved Surfaces

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Horizontal force on vertical surface:

$$F_H = F_x = P_{avg}A = \rho gh_C A = \rho g(s + R/2)A$$

 $= (1000 \text{ kg/m}^3)(9.81 \text{ m/s}^2)(4.2 + 0.8/2 \text{ m})(0.8 \text{ m} \times 1 \text{ m}) \left(\frac{1 \text{ kN}}{1000 \text{ kg} \cdot \text{m/s}^2}\right)$ = 36.1 kN

Vertical force on horizontal surface (upward):

$$F_{y} = P_{avg}A = \rho gh_{c}A = \rho gh_{bottom}A$$
  
= (1000 kg/m<sup>3</sup>)(9.81 m/s<sup>2</sup>)(5 m)(0.8 m × 1 m)  $\left(\frac{1 \text{ kN}}{1000 \text{ kg} \cdot \text{m/s}^{2}}\right)$   
= 39.2 kN





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Weight (downward) of fluid block for one m width into the page:

$$W = mg = \rho g V = \rho g (R^2 - \pi R^2/4)(1 \text{ m})$$

 $= (1000 \text{ kg/m}^3)(9.81 \text{ m/s}^2)(0.8 \text{ m})^2(1 - \pi/4)(1 \text{ m})\left(\frac{1 \text{ kN}}{1000 \text{ kg} \cdot \text{m/s}^2}\right)$ = 1.3 kN

Therefore, the net upward vertical force is

$$F_V = F_y - W = 39.2 - 1.3 = 37.9 \,\mathrm{kN}$$

Then the magnitude and direction of the hydrostatic force acting on the cylindrical surface become

$$F_R = \sqrt{F_H^2 + F_V^2} = \sqrt{36.1^2 + 37.9^2} = 52.3 \text{ kN}$$

$$\tan \theta = F_V / F_H = 37.9 / 36.1 = 1.05 \rightarrow \theta = 46.4^\circ$$





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# To find the weight of the cylinder per m length of the cylinder. Taking a moment about point A at the location of the hinge and equating it to zero gives







## **Force to pressure vessels**

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### Cylindrical pressure vessel







## **Force to pressure vessels**

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### Cylindrical pressure vessel



the stress  $\sigma_1$  is called circumferential stressor the hoop stress, and the stress  $\sigma_2$  is called the longitudinal stress or the axial stress.





## **Force to pressure vessels**

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**Cylindrical pressure vessel** Equilibrium of forces to find the circumferential stress:

$$2lt \,\sigma_1 = 2lrp \implies \sigma_1 = \frac{pr}{2t}$$

Equilibrium of forces to find the longitudinal stress

$$\frac{2\pi rt\sigma_2 = \pi r^2 p}{\sigma_2 = 2\sigma_1} \quad \Rightarrow \quad \sigma_2 = \frac{pr}{t}$$





We note that the longitudinal welded seam in a pressure tank must be twice as strong as the circumferential seam.





## **Force to pressure vessels**

### Spherical pressure vessel

 $F = \pi p r^{2}$ Horizontalforce =  $\sigma (2\pi r_{m})t$ 

$$r_m = r + \frac{t}{2}$$
$$\sigma (2\pi r_m)t = p\pi r^2$$

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$$\sigma = \frac{p r}{2t}$$

Welded seam

$$F = p\pi r^2$$





## **Buoyancy and Stability**

## **Archimedes' Principle**

Fluid pressure acts all over the wetted surface of a body floating in a fluid, and the resultant pressure acts in a vertical upward direction. This force is called buoyancy.

The buoyancy of air is small compared with the gravitational force of the immersed body, so it is normally ignored.

The force  $F_1$  acting on the upper surface is

$$F_1 = (p_0 + \rho g h_1) A$$

The force  $F_2$  acting on the lower surface is

$$F_2 = (p_0 + \rho g h_2) A$$

So, when the volume of the body in the liquid is V, the resultant force F from the pressure acting on the whole surface of the body is

$$F = F_2 - F_1 = \rho g(h_2 - h_1)A = \rho ghA = \rho gV$$









## **Pressure Distribution in Rigid-Body Motion**

#### Equiaccelerated straight-line motion

minute element of mass m on the liquid surface, where its acceleration is  $\alpha$ ,







## **Pressure Distribution in Rigid-Body Motion**

#### **Rotational motion**

$$\tan\phi = \frac{mr\omega^2}{mg} = \frac{r\omega^2}{g}$$

but also

Therefore,

Putting c as a constant of integration,

$$z = \frac{\omega}{2g}r^2 + c$$

 $\tan\phi = \frac{\mathrm{d}z}{\mathrm{d}r}$ 

 $\frac{\mathrm{d}z}{\mathrm{d}r} = \frac{r\omega^2}{g}$ 

If 
$$z = h_0$$
 at  $r = 0, c = h_0$ 

$$z-h_0=\frac{\omega^2 r^2}{2q}$$







## **Example 2:** Pressure Distribution in Rigid-Body Motion

The coffee cup in the following figure is removed from the drag racer, placed on a 3 cm turntable, and rotated about its central axis until a rigid-body mode occurs. Find (a) the 7 cm angular velocity which will cause the coffee to just reach the lip of the cup and (b) the gage pressure at point *A* for this condition.







## **Example 2:** Pressure Distribution in Rigid-Body Motion

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The cup contains 7 cm of coffee. The remaining distance of 3 cm up to

the lip must equal the distance h/2 in Figure (2.16). Thus from Eq. (2.43)

$$h = 2(0.03(m)) = \frac{\omega^2}{2g}r^2 = \frac{\omega^2(0.03(m))^2}{2(9.81(m/s^2))}$$

Solving, we obtain

$$\omega^2 = 1308$$
 or  $\omega = 36.2 rad/s$ 

Where 
$$\omega = \frac{2\pi N}{60}$$
 (N: revolution per minute)  
 $36.2 = \frac{2\pi N}{60} \rightarrow N = 345 rpm$ 

Ans. (a)





## **Example 2:** Pressure Distribution in Rigid-Body Motion

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To compute the pressure, it is convenient to put the origin of coordinates r and z at the bottom of the free-surface depression, as shown in Figure (E2.8). The gage pressure here is  $p_0=0$ , and point **A** is at (r, z) = (3 cm, -4 cm). Equation (2.44) can then be evaluated

$$p = \frac{1}{2} \rho r^2 \omega^2 + p_1 + p_0 = \left[ 0.5 \left( 1010 \left( kg / m^3 \right) \left( 0.03(m) \right)^2 \left( 36.2 \left( rad / s \right) \right)^2 \right] - \left[ \left( 1010 \left( kg / m^3 \right) \left( 9.81(m / s^2) - \left( 0.04(m) \right) \right] + 0 = 990 Pa \right]$$

Ans. (b)

This is about 43 percent greater than the still-water pressure  $p_A = 694$  Pa.





#### Quiz



## Q (2)

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Two water tanks are connected to each other through a mercury manometer with inclined tubes, as shown in the following figure. If the pressure difference between the two tanks is 20 kPa, calculate a and  $\theta$ .









#### Homework



## Hw (3)

Find the net hydrostatic force per unit width on the rectangular gate AB in the following figure and its line of action.





