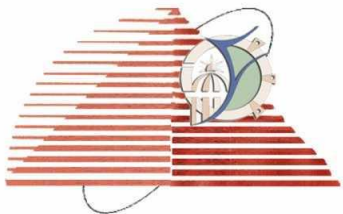


بِسْمِ اللَّهِ الرَّحْمَنِ الرَّحِيمِ



Fayoum University



**Faculty of Engineering
Mechanical Engineering Dept.**

Lecture (5)

on

***The Vibrations of Systems Having
Single Degree of Freedom-
Response to Harmonic and
Periodic Excitations***

By

Dr. Emad M. Saad

Mechanical Engineering Dept.

Faculty of Engineering

Fayoum University

2015 - 2016



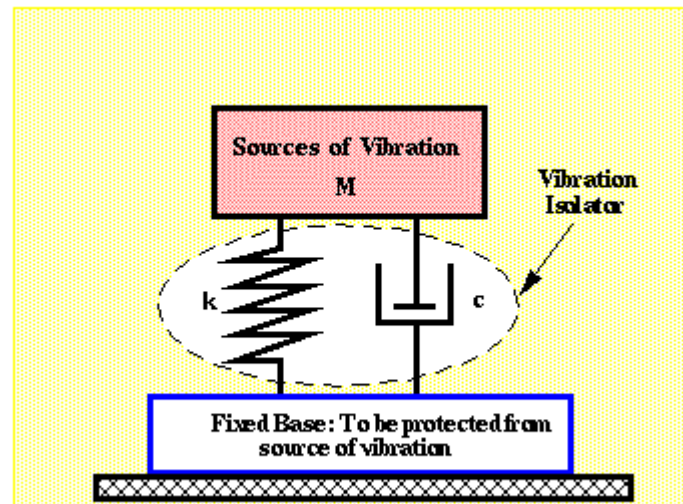
Transmissibility

3

The coefficient of transmissibility is

$$\tau = \frac{F_{tr,max}}{F_{0,max}}$$

Where $F_{tr,max}$ is the maximum transmitted force and $F_{0,max}$ is the maximum perturbation force.



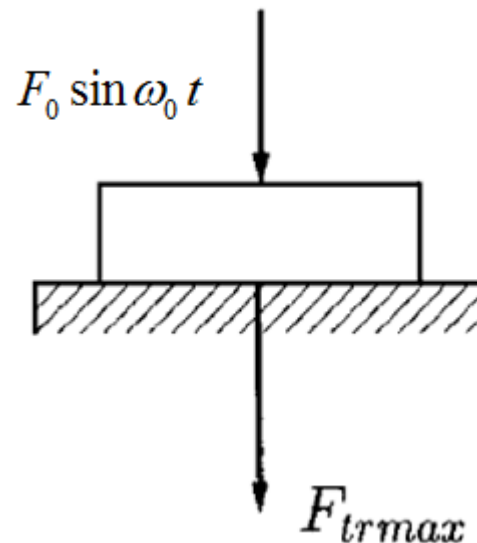


Transmissibility

4

Machine directly on a foundation

In this case (Figure (3.10)), the perturbation force is transmitted to the foundation. The transmissibility coefficient is $\tau = 1$ and the machine is not isolated.



Mechanical model of transmissibility in the case of a machine directly on a foundation.





Transmissibility

5

Machine on a foundation with an elastic element and a damper

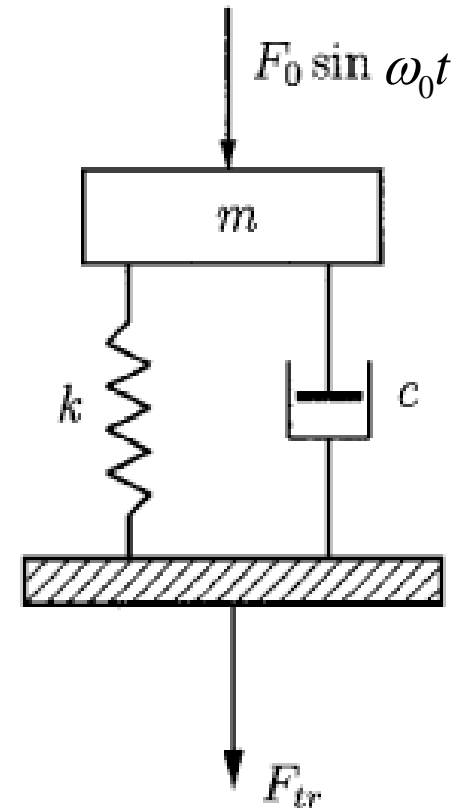
$$m\ddot{x} + c\dot{x} + kx = F_0 \sin \omega_0 t$$

$$x(t) = \frac{F_0}{\sqrt{(k - m\omega_0^2)^2 + c^2 \omega_0^2}} \sin(\omega_0 t - \phi)$$

$$\phi = \tan^{-1} \left[\frac{c\omega_0}{k - m\omega_0^2} \right] \quad \text{Since } \omega_n = \sqrt{k/m} \text{ and } c_{crit} = 2m\omega_n,$$

$$X = \frac{F_0/k}{\sqrt{[1 - (\omega_0/\omega_n)^2]^2 + [2(c/c_{crit})(\omega_0/\omega_n)]^2}}$$

$$\phi = \tan^{-1} \left[\frac{2(c/c_{crit})(\omega_0/\omega_n)}{1 - (\omega_0/\omega_n)^2} \right]$$





Transmissibility

6

Machine on a foundation with an elastic element and a damper

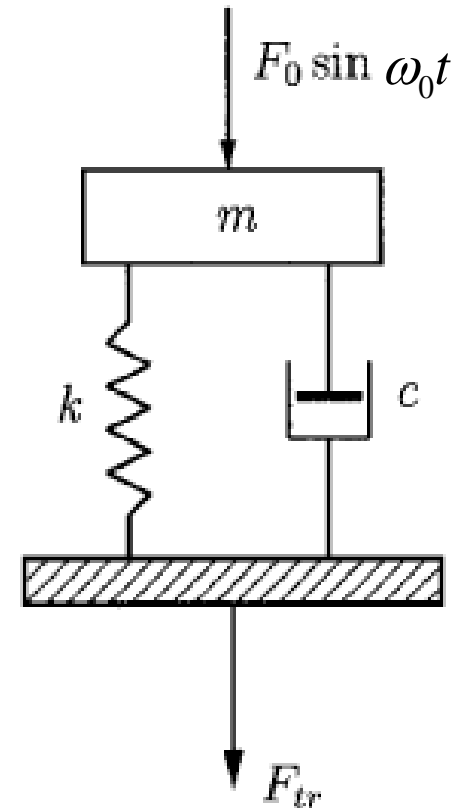
$$m\ddot{x} + c\dot{x} + kx = F_0 \sin \omega_0 t$$

$$x(t) = \frac{F_0}{\sqrt{(k - m\omega_0^2)^2 + c^2 \omega_0^2}} \sin(\omega_0 t - \phi)$$

$$\phi = \tan^{-1} \left[\frac{c\omega_0}{k - m\omega_0^2} \right] \quad \text{Since } \omega_n = \sqrt{k/m} \text{ and } c_{crit} = 2m\omega_n,$$

$$X = \frac{F_0/k}{\sqrt{\left[1 - (\omega_0/\omega_n)^2\right]^2 + \left[2(c/c_{crit})(\omega_0/\omega_n)\right]^2}}$$

$$\phi = \tan^{-1} \left[\frac{2(c/c_{crit})(\omega_0/\omega_n)}{1 - (\omega_0/\omega_n)^2} \right]$$





Transmissibility

Machine on a foundation with an elastic element and a damper

The transmitted force is not in the same phase with the perturbation force. In this case, the transmitted force is

$$F_{tr,max} = [kx + c\dot{x}]_{max}$$

The exciting vibration is

$$x(t) = X \sin(\omega_0 t - \phi)$$

and

$$\dot{x}(t) = X\omega_0 \cos(\omega_0 t - \phi)$$

Therefore, the force transmitted to the foundation is

$$\begin{aligned} F_{tr} &= kx + c\dot{x} \\ &= kX \sin(\omega_0 t - \phi) + cX\omega_0 \cos(\omega_0 t - \phi) \\ &= M \sin(\omega_0 t - \phi) \end{aligned}$$

The magnitude of the total transmitted force is given by

$$M = \sqrt{k^2 X^2 + c^2 X^2 \omega_0^2} = F_{tr,max}$$

which represents the maximum transmitted force.





Transmissibility

8

Machine on a foundation with an elastic element and a damper

The transmissibility coefficient is

$$\begin{aligned} \tau &= \frac{X \sqrt{k^2 + c^2 \omega_0^2}}{F_0} = \frac{\sqrt{\frac{k^2}{m^2} + \frac{c^2 \omega_0^2}{m^2}}}{\sqrt{(\omega_n^2 - \omega_0^2)^2 + 4\omega_0^2 \left(\frac{c}{2m}\right)^2}} = \sqrt{\frac{\omega_n^4 + 4\omega_0^2 \left(\frac{c}{2m}\right)^2}{(\omega_n^2 - \omega_0^2)^2 + 4\omega_0^2 \left(\frac{c}{2m}\right)^2}} \\ &= \sqrt{\frac{1 + \left[4 \left(\frac{c}{2m\omega_n}\right)^2 \left(\frac{\omega_0}{\omega_n}\right)^2\right]}{\left(1 - \frac{\omega_0^2}{\omega_n^2}\right)^2 + \left[4 \left(\frac{c}{2m\omega_n}\right)^2 \left(\frac{\omega_0}{\omega_n}\right)^2\right]}} \end{aligned}$$





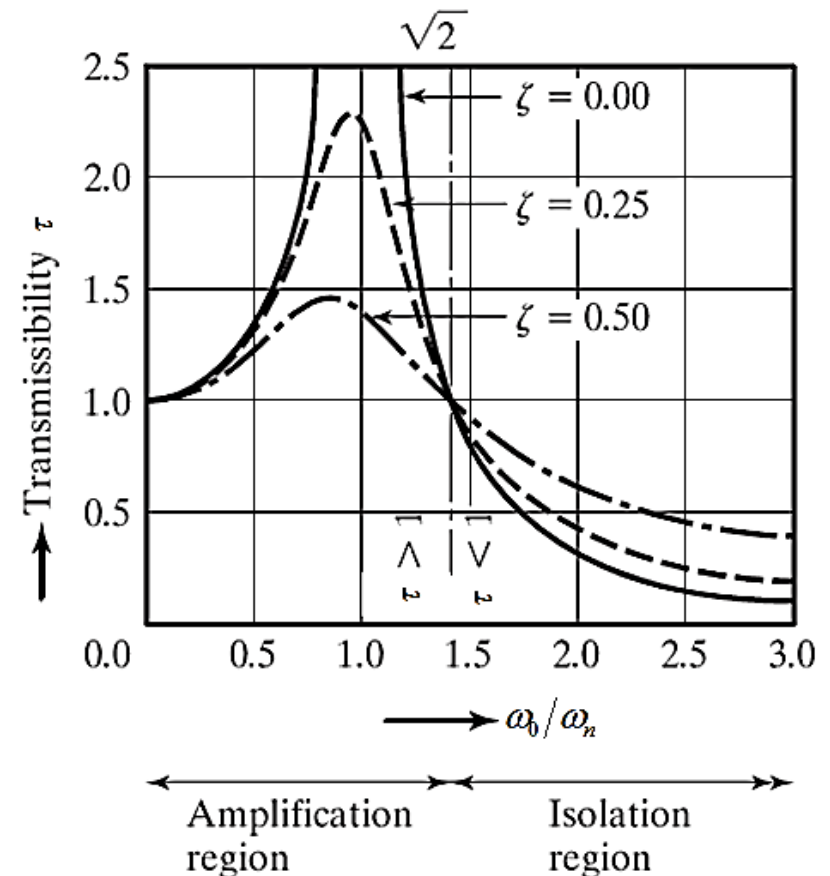
Transmissibility

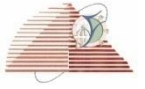
9

Machine on a foundation with an elastic element and a damper

$$\tau = \sqrt{\frac{1 + \left[4 \left(\frac{c}{c_{crit}} \right)^2 \left(\frac{\omega_0}{\omega_n} \right)^2 \right]}{\left(1 - \frac{\omega_0^2}{\omega_n^2} \right)^2 + \left[4 \left(\frac{c}{c_{crit}} \right)^2 \left(\frac{\omega_0}{\omega_n} \right)^2 \right]}}$$

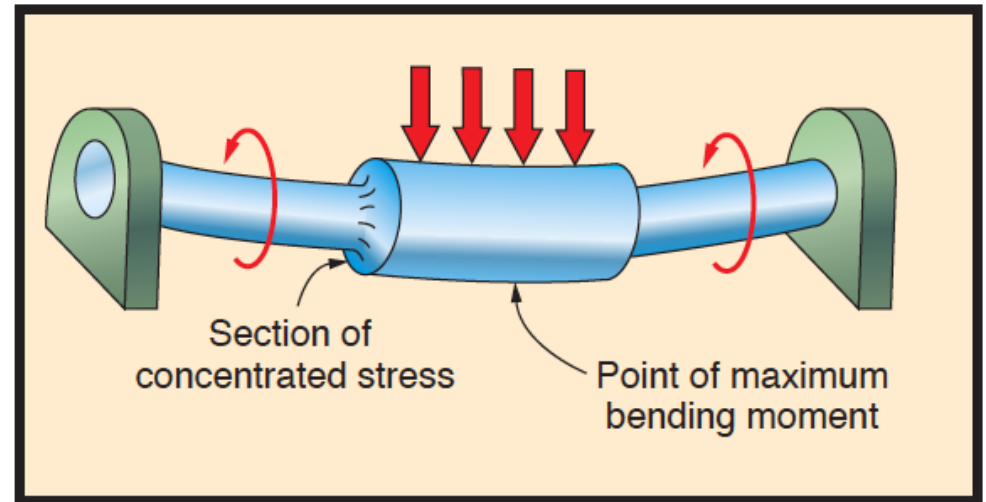
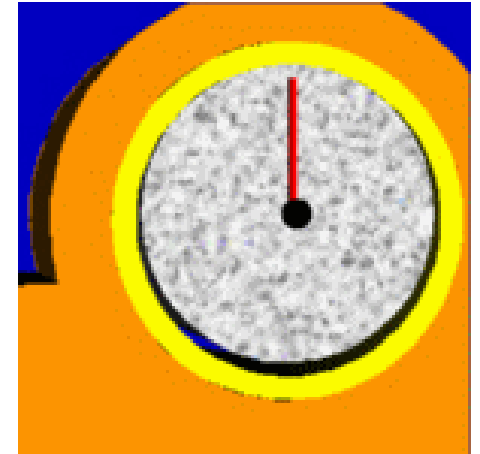
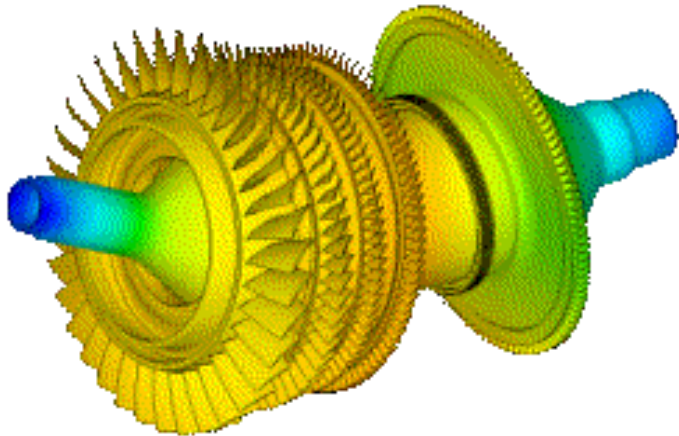
$$= \sqrt{\frac{1 + \left(2\zeta \frac{\omega_0}{\omega_n} \right)^2}{\left(1 - \frac{\omega_0^2}{\omega_n^2} \right)^2 + \left(2\zeta \frac{\omega_0}{\omega_n} \right)^2}}$$





The Whirling of Rotating Shafts

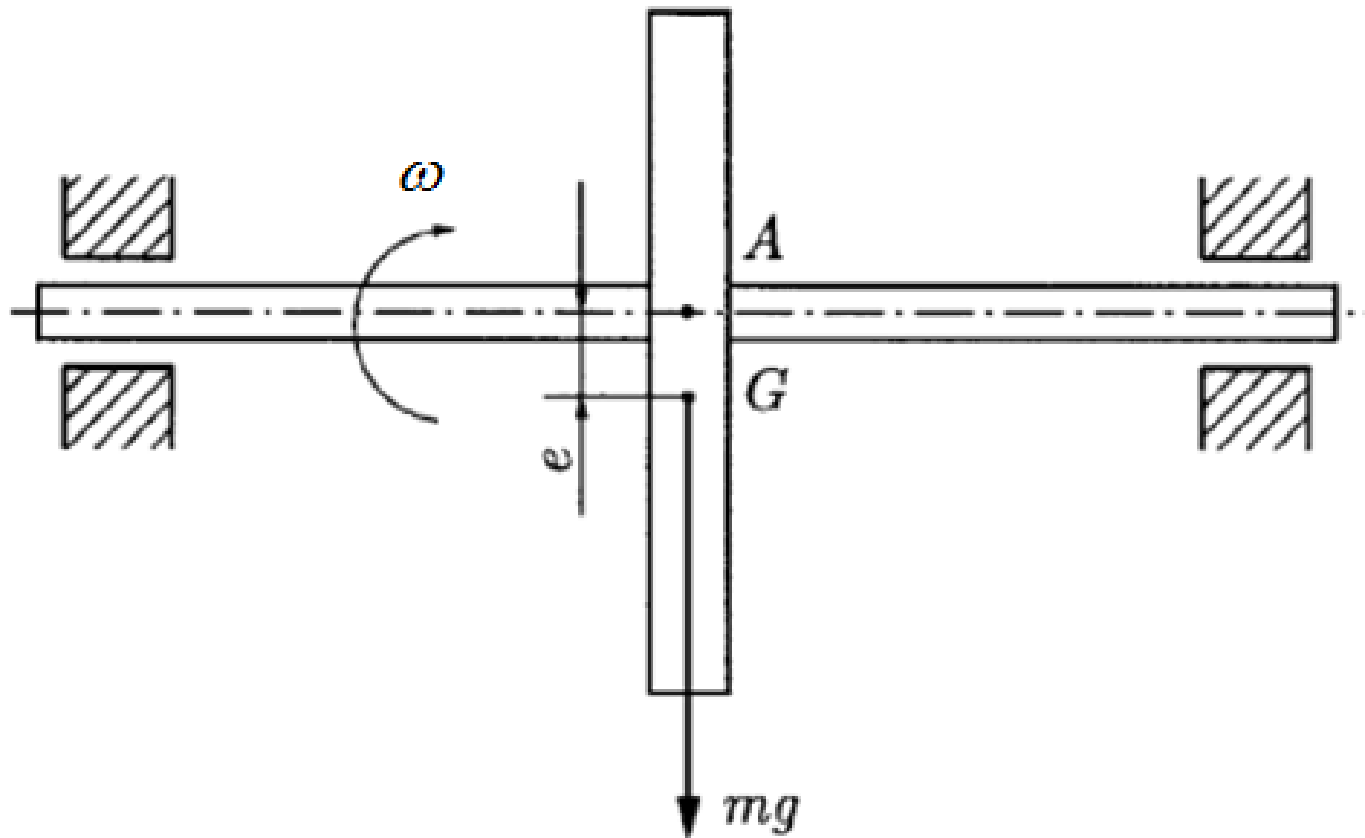
10





The Whirling of Rotating Shafts

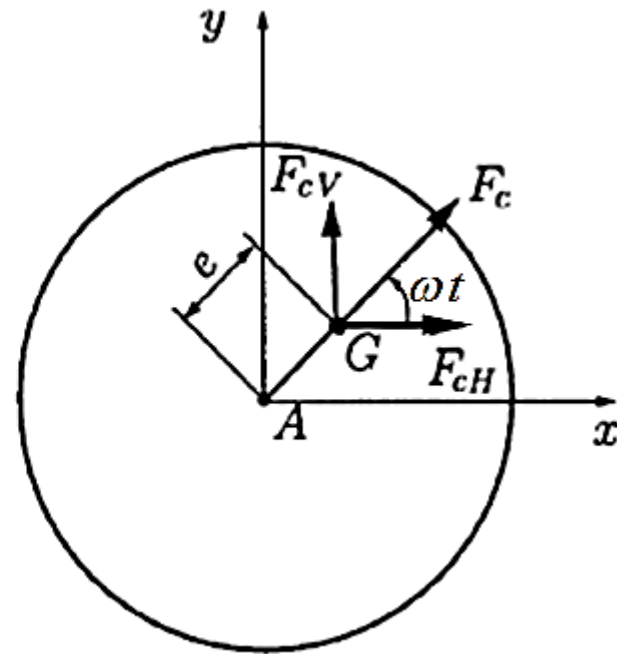
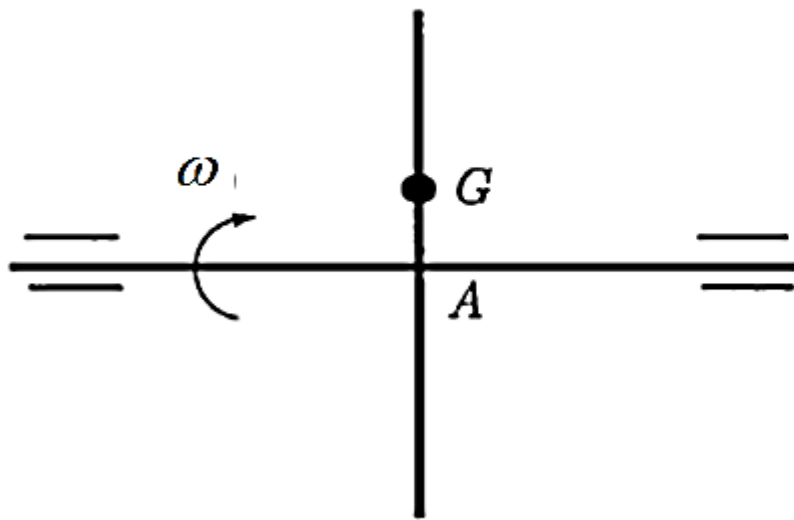
11





The Whirling of Rotating Shafts

12



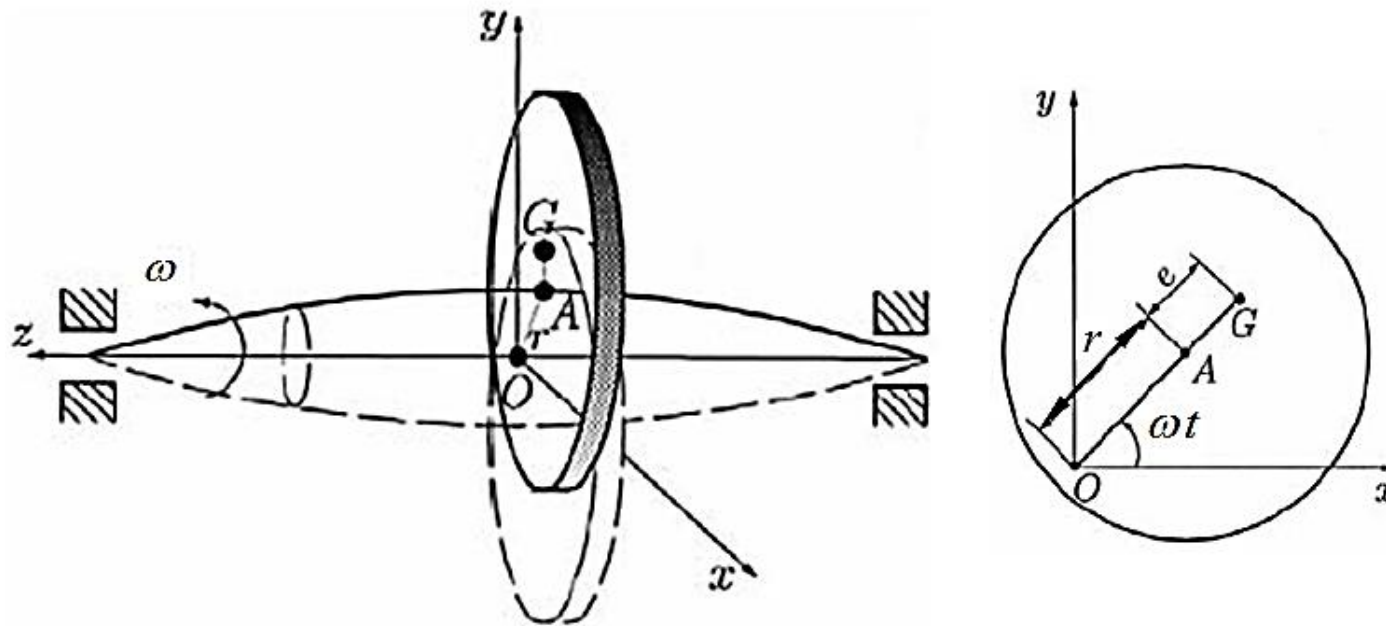
$$\begin{cases} F_{c,H} = me\omega^2 \cos \omega t \\ F_{c,V} = me\omega^2 \sin \omega t \end{cases} \rightarrow \begin{cases} \ddot{x} + \omega_n^2 x = e\omega^2 \cos \omega t \\ \ddot{y} + \omega_n^2 y = e\omega^2 \sin \omega t \end{cases} \text{ and } \omega_n^2 = \frac{k_{eq}}{m}$$





The Whirling of Rotating Shafts

13



The center line of the support bearings intersects the plane of the wheel at O and the shaft center is deflected with $r = OA$.

$$k_{eq} r = m(r + e)\omega^2 = mr\omega^2 + me\omega^2$$





The Whirling of Rotating Shafts

$$r = e \frac{\omega^2}{\left(\frac{k_{eq}}{m}\right) - \omega^2} = e \frac{\left(\frac{\omega}{\omega_n}\right)^2}{1 - \left(\frac{\omega}{\omega_n}\right)^2} \quad k_{eq} = \frac{48EI}{l^3}$$

By analogy with Eq. (3.9) (in case of $\zeta = 0$), Eqs. (3.31) have the solution

$$\begin{cases} x(t) = e \frac{(\omega/\omega_n)^2}{1 - (\omega/\omega_n)^2} \cos \omega t \\ y(t) = e \frac{(\omega/\omega_n)^2}{1 - (\omega/\omega_n)^2} \sin \omega t \end{cases}$$





The Whirling of Rotating Shafts

If the circular frequency of transversal vibration (bending) is equal to the rotation **angular speed**, then the resonance will take place. In this case rotation angular speed is called critical angular speed ω_{crit} , and the critical **rpm** is N_{crit} , given by

$$N_{crit} = \frac{30}{\pi} \omega_{crit}$$

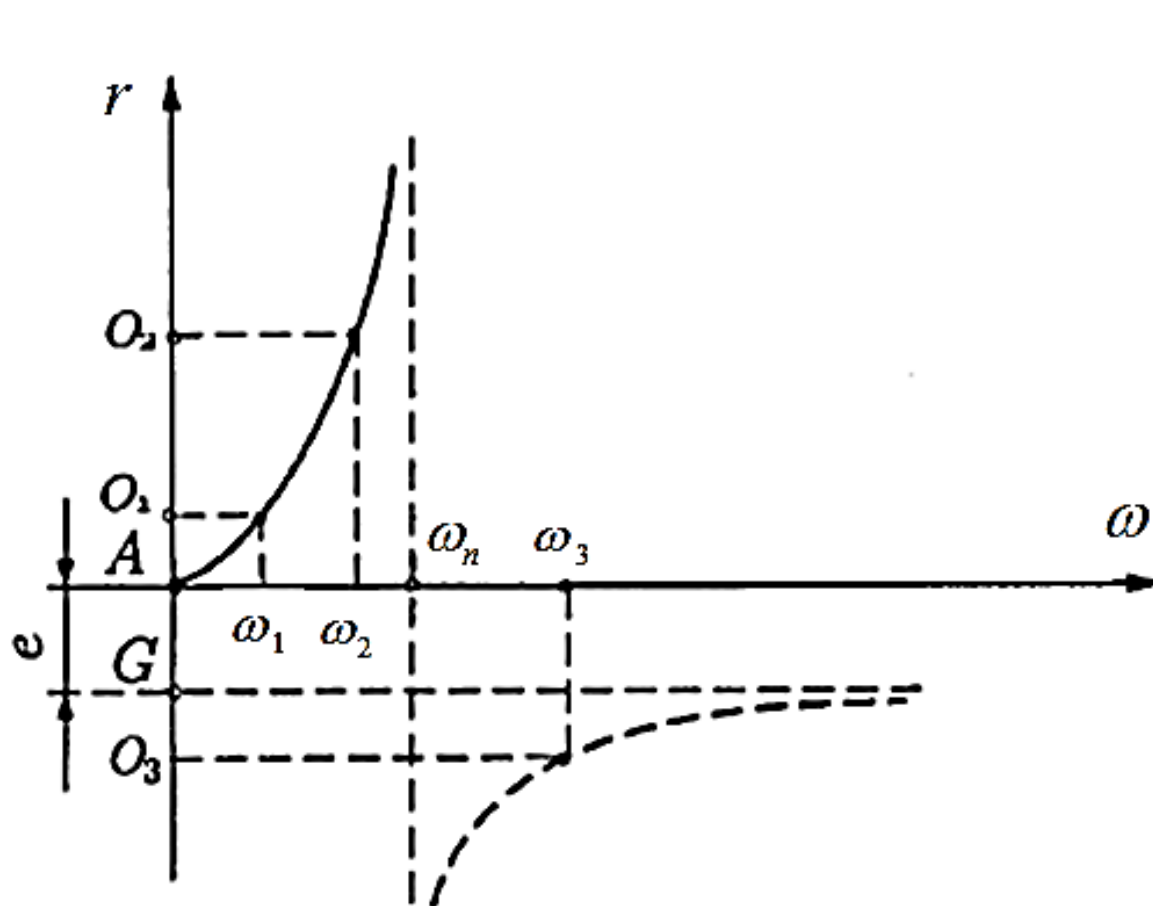
$$N_{crit} = \frac{60}{2\pi} \omega_n = \frac{60}{2\pi} \sqrt{\frac{48EI}{ml^3}} \text{ rpm}$$



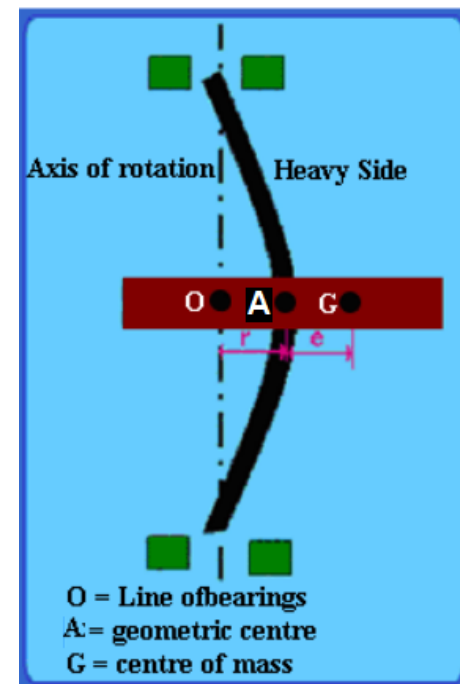


The Whirling of Rotating Shafts

16



$$r = e \frac{\omega^2}{\left(\frac{k_{eq}}{m}\right) - \omega^2} = e \frac{\left(\frac{\omega}{\omega_n}\right)^2}{1 - \left(\frac{\omega}{\omega_n}\right)^2}$$

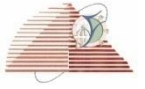




The Whirling of Rotating Shafts

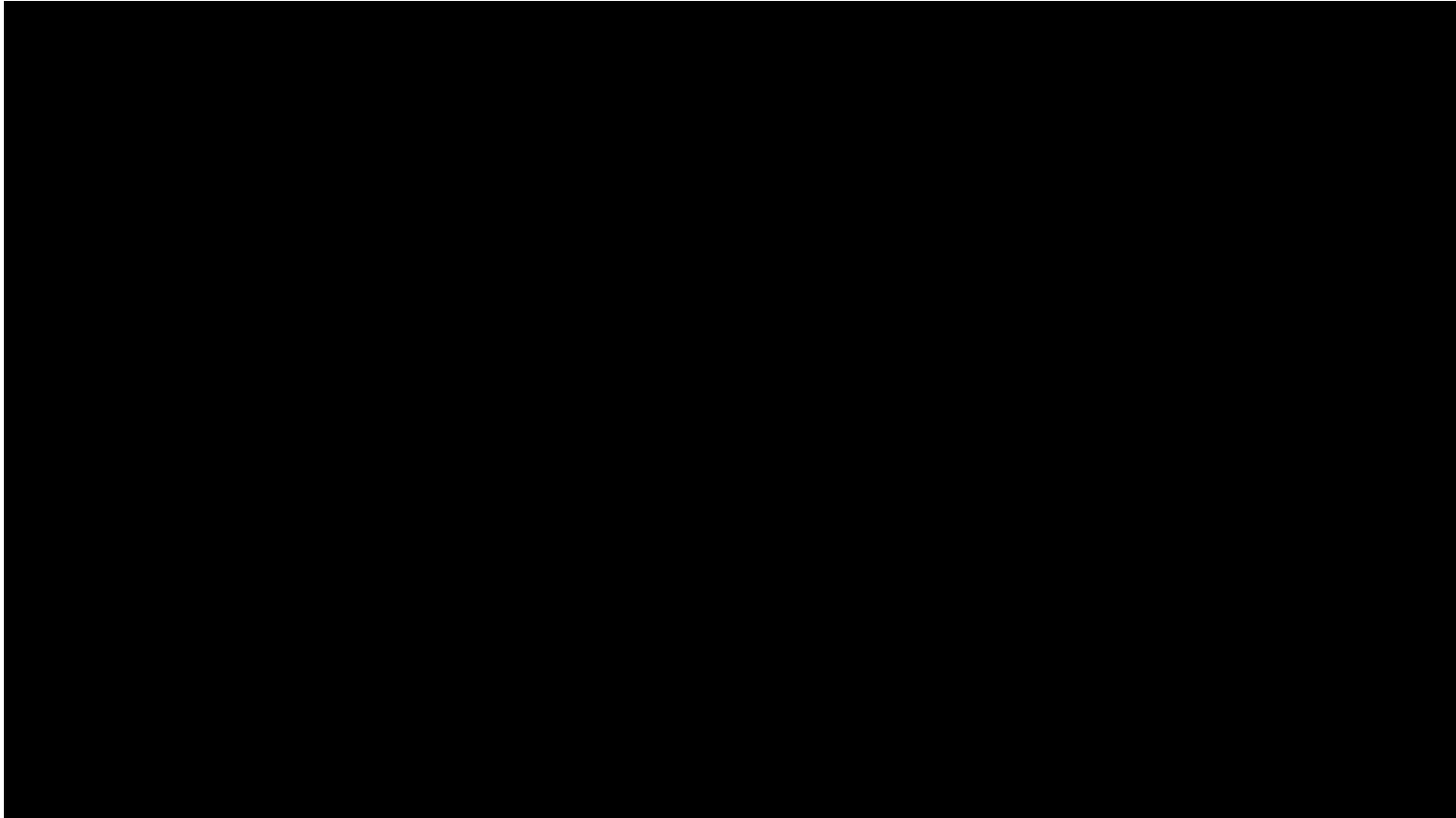
1. One is **undercritical** ($\omega < \omega_n$) when $r > 0$ and the point G is outside of segment OA .
2. The other one is **overcritical** ($\omega > \omega_n$) when $r < 0$ and the point G is inside of segment OA .
3. If **angular speed** of the shaft increases, the point of mass G tends to point O (center line of bearings). This phenomenon is called self-centering or self-aligning.





The Whirling of Rotating Shafts

18





Other Forms of Damping

For a harmonic motion of the form $x(t) = X \sin \omega t$, the energy dissipated over one cycle of motion due to a damping force F_D is

$$\Delta E = \int_0^{2\pi/\omega} F_D \dot{x} dt = \int_0^{2\pi/\omega} F_D X \omega \cos \omega t dt$$

For viscous damping,

$$\Delta E = \int_0^{2\pi/\omega} c \dot{x}^2 dt = \int_0^{2\pi/\omega} c \omega^2 X^2 \cos^2 \omega t dt = c \omega \pi X^2$$

Thus, by analogy, the equivalent viscous damping coefficient for another form of damping is

$$c_{eq} = \frac{\Delta E}{\omega \pi X^2}$$



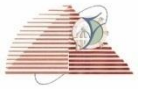


Self-excited Vibration

Self-excited vibrations pervade all areas of design and operations of physical systems where motion or time-variant parameters are involved:

- 1. Aeromechanical systems (flutter, aircraft flight dynamics),**
- 2. Aerodynamics (separation, stall, musical wind instruments, diffuser and inlet chugging),**
- 3. Aerothermodynamics (flame instability, combustor screech),**
- 4. Mechanical systems (machine-tool chatter),**
- 5. Feedback networks (pneumatic, hydraulic, and electromechanical servomechanisms).**

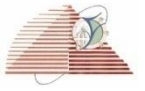




Self-excited Vibration

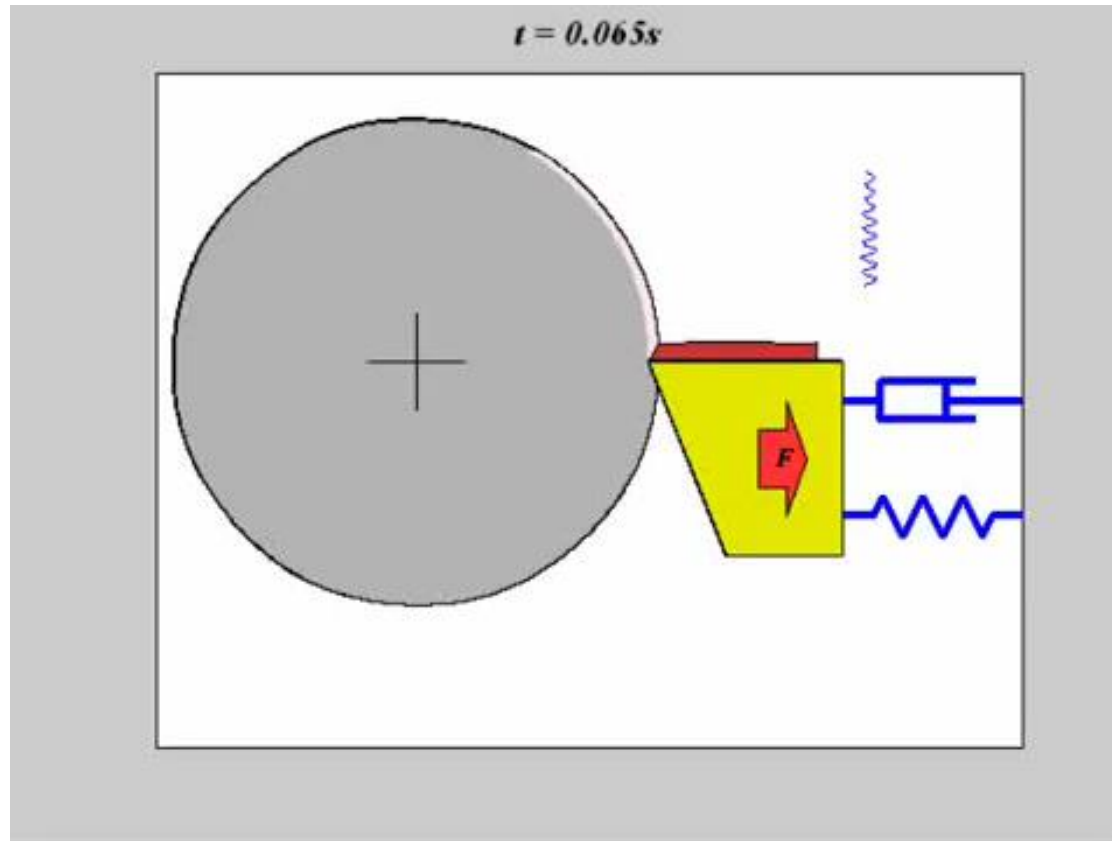
21





Self-excited Vibration

22

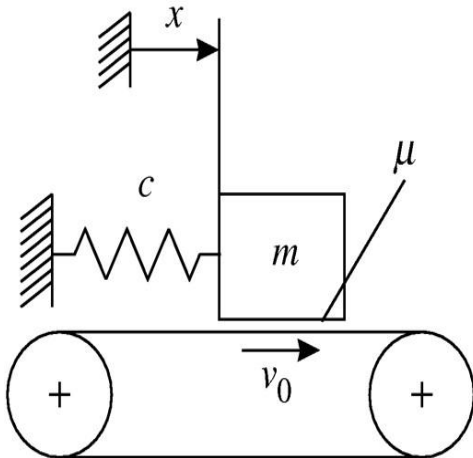




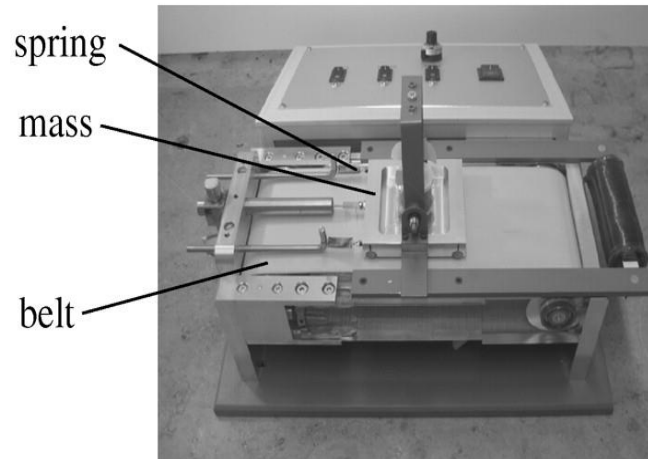
Self-excited Vibration

23

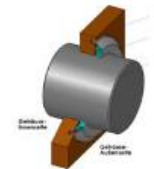
(a)



(b)



vehicle brakes



shaft seals



band saws



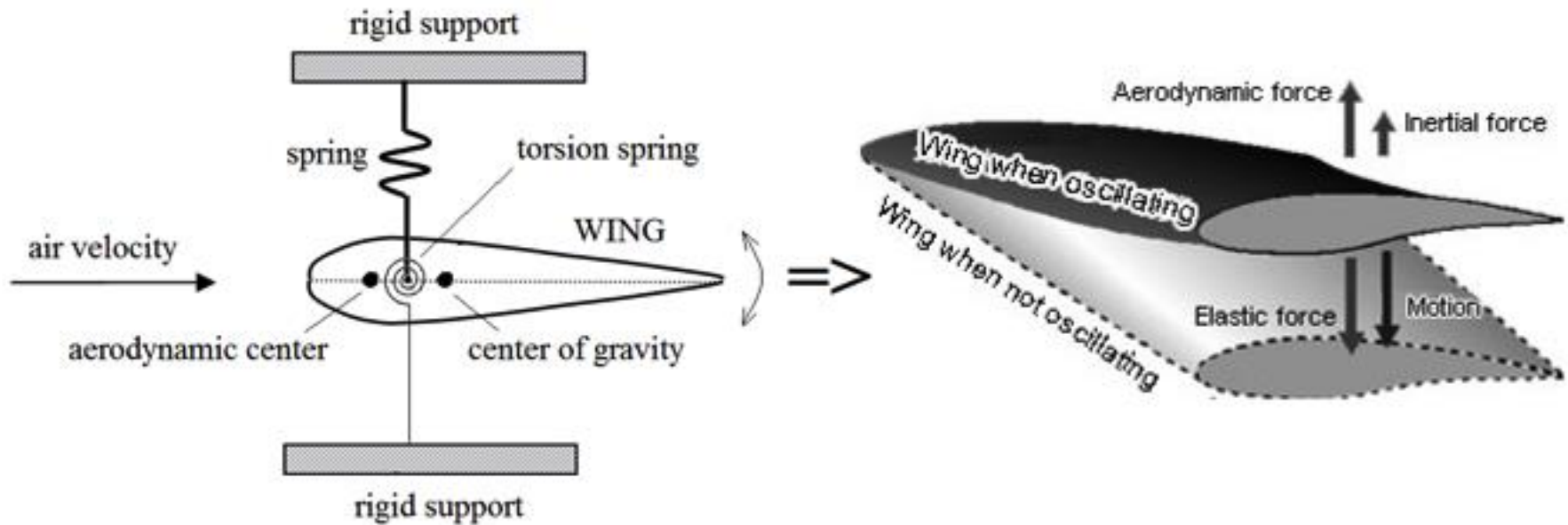
grinding tools

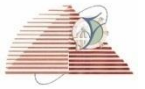




Self-excited Vibration

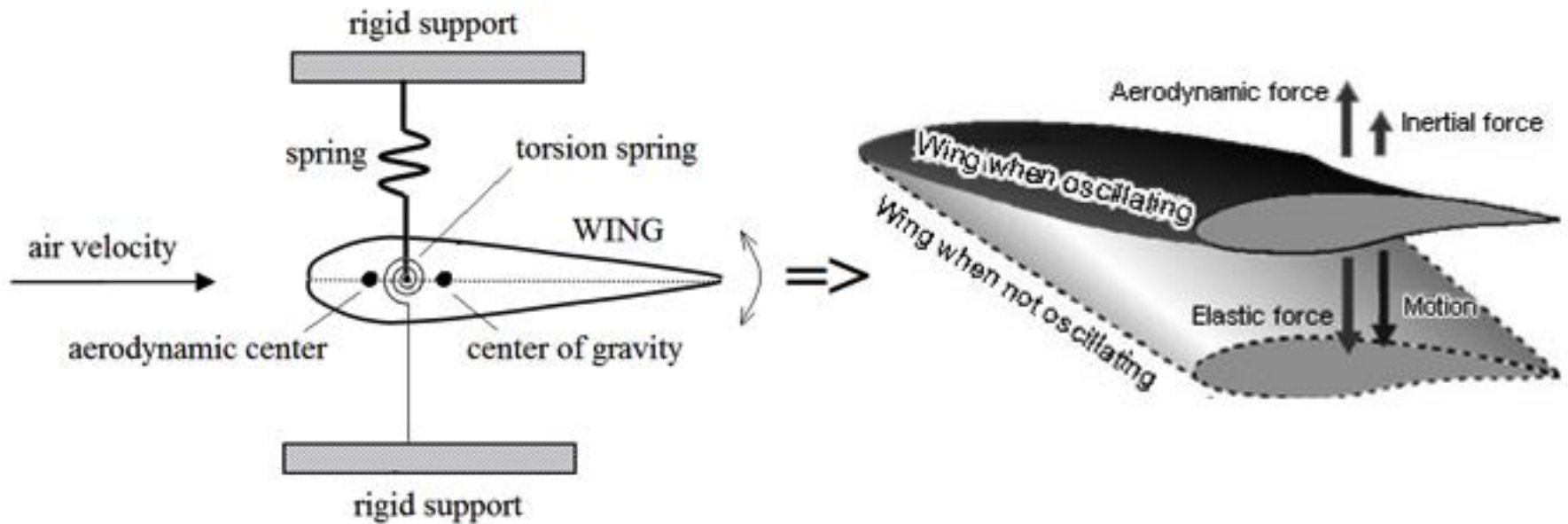
24



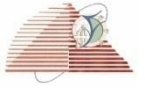


Self-excited Vibration

25







Quiz

27

A steel shaft of diameter 2.5 cm and length 1 m is supported at the two ends in bearings. It carries a turbine disc, of mass 20 kg and eccentricity 0.005 m, at the middle and operates at 6000 rpm. The damping in the system neglected. Determine the whirl amplitude of the disc at (a) operating speed, (b) critical speed, and (c) 1.5 times the critical speed.



Thank
You